Evaluation of Low-volume Sprayers Used in Asian Citrus Psyllid Control Applications

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Summary. The asian citrus psyllid [Diaphorina citri (Sternorrhyncha: Psyllidae)] is a detrimental pest to citrus (Citrus spp.) crops when it serves as a vector of the pathogen that causes greening (huanglongbing). Transmission of this disease causes mottling, chlorosis, dieback, and reductions in fruit size and quality. Citrus producers have found that many pesticides, when applied properly, are very effective at suppressing or eliminating asian citrus psyllids in groves. Due to the threat of greening, several pesticides have been granted Special Local Needs registration for use in the state of Florida if the product is sprayed with a volume median diameter of 90 µm or greater. A number of studies involving numerous citrus sprayers and a.i. were conducted to determine the droplet sizes generated by different sprayers operating under user-established settings and the adjustments required to those settings for the sprayers to meet the 90-um requirement. In the sprayer tests, it was found that reductions in engine speed or increases in flow rate were required to increase droplet sizes to meet the product label-required droplet size. As the equipment tested here represent the most typical application equipment used in Florida for asian citrus psyllid control, these results will provide applicators, growers, and extension agents with general guidelines to ensure that spray systems are operated in a manner that complies with label restrictions.

he asian citrus psyllid is a detrimental pest to citrus crops when it serves as a vector of the pathogen that causes greening [huanglongbing (HLB)]. Transmission of this disease causes mottling, chlorosis, dieback, and reductions in

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⁸Corresponding author. E-mail: clint.hoffmann@ars. usda.gov. fruit size and quality (Halbert and Manjunath, 2004). Once a tree is infected, there is no cure, and trees may only live for another 5 to 8 years, potentially never bearing usable fruit. It is well established that the presence of asian citrus psyllids and the vectored pathogen necessitate chemical control in the form of pesticide applications (Tolley, 1990). Given the seriousness of the disease, it is important to protect even apparently disease-free trees (Aubert, 1990), especially with new growth flush (Aubert 1987). Recommended treatment intervals range from 10 to 13 treatments per year (Roistacher, 1996) to every 7 to 20 d (Gonzales and Viñas, 1981), with area-wide treatments being preferred (Aubert 1990). Supriyanto and Whittle (1991) recommend high-efficacy pesticides as essential to provide sufficient control to significantly delay a greening epidemic. It can be further conjectured that optimal application techniques also are critical to obtaining maximum biological control of asian citrus psyllids.

Stover et al. (2002), in a survey to indentify current spray application practices on citrus crops in Florida, identified three predominate sprayer types, including two airblast sprayers at mid- and high-volume application rates and a low-volume application rate air-assisted sprayer, with spray rates ranging from 25 to 750 gal/ acre. Sprayer type is generally selected by the operator based on experience and/or perceived coverage and deposition of spray material within the citrus canopy. The selected sprayers can typically be modified to generate spray plumes that fit tree contours through changes in nozzle numbers, and orientation of and/or oscillation of airflow (Stover et al., 2003). With the need for numerous spray treatments for asian citrus psyllid control, applicators are looking to and adapting for use a number of spray application machines initially targeted for the mosquito vector control industry. Machines that apply agrochemical products at these low-volume rates allow applicators to respond to the need to treat large numbers of acres repeatedly in a timely manner. These machines can produce droplets with volume median diameters that range from 5 to 210 µm, depending on spray solution and equipment setup (Hoffmann et al., 2007a).

The list of pesticides approved for application to control asian citrus psyllids in Florida is limited. As a result of the urgent need for control, applicators in Florida have been granted Special Local Needs provisions on a number of insecticides, including spinetoram (Delegate® WG; Dow

Units			
To convert U.S. to SI, multiply by	U.S. unit	SI unit	To convert SI to U.S., multiply by
0.3048	ft	m	3.2808
3.7854	gal	L	0.2642
9.3540	gal/acre	$L \cdot ha^{-1}$	0.1069
2.54	inch(es)	cm	0.3937
1	micron	μm	1
0.4470	mph	$\dot{\mathrm{m}}\cdot\mathrm{s}^{-1}$	2.2369
70.0532	oz/acre	g∙ha ⁻¹	0.0143
6.8948	psi	kPa	0.1450

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Form Approved OMB No. 0704-0188 AgroSciences, Indianapolis), diflubenzuron (Micromite® 80WGS; Chemtura, Middlebury, CT), fenpropathrin (Danitol 2.4 EC; Valent, Walnut Creek, CA), and zeta-cypermethrin (Mustang; FMC, Philadelphia). All of these Special Local Needs labels require air-blast or air-assisted sprayers with application rates of no less than 2 gal/acre and with volume median droplet diameters of 90 µm or larger. Most labels allow the addition of adjuvants or other tank-mix partners as long as the other restrictions are maintained; however, fenpropathrin does not allow use of additional adjuvants. No information is given regarding the reasoning behind the 90-µm lower limit, though it is likely based on risk assessment analysis for spray drift. The Special Local Needs labels also do not specify an upper limit on the droplet size. Given that spray droplet size is dependent on and changes with varying combinations of spray equipment, equipment setup, and spray product (Hoffmann et al., 2007b), the objectives of this work were: 1) evaluate three sprayers, under laboratory conditions, for droplet size produced from a.i. formulations and the necessary equipment adjustments needed to meet the Special Local Needs label; 2) conduct "onsite" evaluations of production application equipment for droplet size when operating under normal conditions; 3) adjust the individual sprayer's operating parameters to produce a volume median diameter of 90 µm or greater to ensure compliance with the Special Local Needs labels; and 4) document the general operational modifications required for machine type to provide guidance for future spray calibrations.

Materials and methods

Sprayer droplet size testing was completed in two stages: one looking at three sprayers and five a.i. under laboratory conditions and the second, a field-based evaluation of production sprayers brought to a central location by local applicators. The first laboratory-based work was conducted at the U.S. Department of Agriculture-Agricultural Research Service (USDA-ARS) Areawide Pest Management Research Unit's Riverside campus facilities in College Station, TX. The three sprayers to be evaluated were provided by the equipment manufacturers. The

field-based evaluations were conducted at two locations in central Florida. Both sets of trials followed the same testing protocols with the exception of the field-based trials not using a.i. formulations. These procedures, along with greater details on the site-specific testing, are discussed further in the following sections.

GENERAL TESTING PROCEDURES. To evaluate the droplet size produced by a particular sprayer and spray formulation combination, the sprayer was first operated under its normal factory or user-established settings. Basically, the sprayer was initially operated as-is. A droplet measurement system (Sympatec, Clausthal, Germany) mounted on a custom-made forklift mount was used to measure droplet size at the sprayer nozzle outlet. The unit was positioned such that the location of measurement was ≈ 1 to 2 m from the outlet of the sprayer (Fig. 1). This distance varied somewhat from sprayer to sprayer depending on the droplet density of the resulting spray cloud and the width of the spray plume. Wider spray plumes required a closer distance to avoid depositing spray material on the lenses of the droplet measurement unit. Denser sprays required further distance to insure that the spray cloud density did not prevent the diffracted laser light from reaching the measurement sensor. The spray cloud from the sprayer was directed through the laser beam for 10 to 20 s during which time droplet size measurements of the spray cloud were made. The time that the spray cloud was directed through the optical path of the laser varied between sprayers depending on the width of the spray plume generated by the sprayer. The

entire spray plume for each sprayer was measured by traversing the laser through the plume using the forklift (ASTM International, 2009). Three replicated measures were made for each unique piece of equipment and specific set of operational conditions.

Droplet sizing system. The Helos laser diffraction droplet sizing system (Sympatec), which uses a 623nm helium-neon laser, was fitted with an R5 lens, resulting in a dynamic size range from 0.5 to 875 µm in 32 sizing bins. The authors found that when using the laser system under adverse conditions (outdoors and mounted to a forklift), the last channel (i.e., sizing bins) of the Helos system should be turned off such that it is not factored into the droplet size measurement results. This channel represents the largest droplet size and tends to pick up some "noise" or random signals that typically result from equipment vibration or scattered ambient light. With this channel turned off, the dynamic range of the instrument was from 0.5 to 735 µm. These channels were not turned off if any droplets were measured within two sizing bins of the nearest deactivated channel.

The spray droplet size data were determined and reported as a mean and standard deviation corresponding to the data measured during the three replications for each combination of sprayer and pesticide. Means and standard deviations of the volume median diameter [VMD or $D_{V0.5}$ (ASTM International E1620-97, 2004)], $D_{V0.1}$, and $D_{V0.9}$ were determined. The $D_{V0.5}$ is the droplet diameter in micrometers where 50% of the spray volume is contained in droplets smaller than this value (ASTM



Fig. 1. Testing setup showing the droplet measurement system with the spray plume from the citrus sprayer directed through the laser beam of the droplet measurement system.

Standard E1620, 2004). Similarly, the $D_{V0.1}$ and $D_{V0.9}$ values are the diameters at which 10% and 90%, respectively, of the spray volume is contained in droplets of these sizes.

ACTIVE INGREDIENT TESTS. For the laboratory studies, five a.i. along with water plus a nonionic surfactant (NIS) were used. The use of a specially designed scrubbing system allowed for the use of these a.i. without adverse environmental impacts. Three liquid-based products were used: malathion (Malathion 5EC; Drexel Chemical, Memphis, TN), dimethoate (Dimethoate 4E; Arysta Life-Science North America, Cary, NC), and fenpropathrin. Two of the products were wettable powders: diflubenzuron and spinetoram. The rates at which these products were tested are shown in Table 1. For all a.i. tests, spray rates were maintained at 3 gal/ acre. For each of the three sprayers tested, the first step was to run the sprayer at the factory settings using water to determine a benchmark for further modifications. Depending on the measured $D_{V0.5}$, engine speed was modified such that the 90-µm lower size requirement was met. The goal for each a.i. formulation tested was to determine the appropriate engine speed settings that resulted in compliance with the Special Local Needs permit.

CITRUS SPRAYER CALIBRATION RODEOS. The field evaluations were organized by the Florida Extension Service in Lake Placid, FL, and Haines City, FL. Growers and applicators in the region were invited to bring their equipment to these locations for droplet size measurements. Thirty-three machines were evaluated representing

Table 1. Five a.i. (three liquid and two wettable powders) and the rates at which they were used in the sprayer calibration trials.

Liquid formulation	Application rate (oz/acre a.i.) ^z
Malathion Dimethoate	9.0 13.9
Fenpropathrin	6.2
Wettable powders	Application rate (oz/acre a.i.)
Diflubenzuron	5.0
Spinetoram	1.0

 $^{^{}z}1 \text{ oz/acre} = 70.0532 \text{ g·ha}^{-1}.$

16 different models of sprayers. Water with 0.25% volume/volume addition of a NIS (R-11; Wilbur-Ellis, Walnut Creek, CA) was used during these tests as there were a large number of spray trials conducted and a large number of people involved. This prevented any environmental contamination or adverse health effects. The water plus NIS solution simulates most water-based insecticide sprays well (Hoffmann et al., 2007a, 2007b). Each sprayer tested was initially run at the user settings. Based on the measured D_{V0.5}, engine speed and, in a few cases, sprayer pressure were adjusted until the 90µm size requirement was met. Typically, engine speed was first reduced to its minimum level and if the resulting measured $D_{V0.5}$ was still less than 90 µm, spray pressure was increased.

An example of the data reports that were provided to each of the applicators is shown in the Appendix (Fig. 2).

Results

ACTIVE INGREDIENT TESTS WITH THREE SPRAYERS. Final equipment settings required to meet the $D_{V0.5}$ 90um size requirement for each a.i. are shown in Tables 2 through 4 for the three sprayers tested. Droplet size at the factory settings for water and water plus NIS are also included for reference. For the London Fog model 18–20 sprayer (London Fog, Long Lake, MN) (Table 2), initial testing with water and water plus NIS with the machine operating at 2810 and 1850 rpm, respectively, and a rate of 1.9 L·min⁻¹ produced $D_{V0.5}$ of 57.8 ± 13.2 and 85.9 \pm 1.2 μ m (mean \pm sD of three replications), respectively. Two of the a.i. formulations, diflubenzuron and spinetoram, produced D_{V0.5} values that were at or near the 90-µm requirement while operating the sprayer at 1500 rpm while two, fenpropathrin and malathion, required reducing the engine speed to 1350 rpm. The dimethoate formulation was such that even at the lowest engine speed setting (1350 rpm), the 90-µm size requirement could not

For the Curtec sprayer (Curtec of Florida, Vero Beach, FL), water and water plus NIS resulted in $D_{V0.5}$ that were greater than 90 μ m at factory settings. Dimethoate and

diflubenzuron formulation also achieve the 90-µm requirement at the factory settings, while the malathion, spinetoram, and fenpropathrin formulation required engine speeds to be reduced to 4800, 4000, and 4000 rpm, respectively.

For the Proptec sprayer (Ledebuhr Industries, Williamston, MI), water and water plus NIS resulted in $D_{V0.5}$ values that met the 90- μ m requirement. Spinetoram and diflubenzuron formulations also met the 90- μ m requirement at the 5100-rpm factory setting, while malathion and fenpropathrin formulations required the engine speed to be reduced to 3500 rpm.

CITRUS SPRAYER CALIBRATION RODEOS: SINGLE MACHINE EVALUATIONS. During the calibration rodeos, there were 17 unique models of machines evaluated. Fourteen of the models only had one machine of that type that was tested. Two, the Dyna-Fog Ag-Mister LV-8 (Curtis Dyna-Fog, Westfield, IN) and the London Fog model 18–20, had multiple machines of that type tested.

Of the individual machines tested, eight had a $D_{V0.5}$ of 90 um or greater (Table 5). Three of the remaining sprayers were able to be adjusted via spray pressure or engine speed to achieve a $D_{V0.5}$ near or greater than 90 μ m. One of the sprayers, MaxCharge ES100 (Electrostatic Spraying Systems, Watkinsville, GA), was designed to generate droplets with a $D_{V0.5}$ of between 30 and 40 μ m to optimize the electrostatic charge that it imparts to the spray droplets.

There were 14 Dyna-Fog Ag-Mister LV-8 (LV-8) and six London Fog model 18–20 citrus sprayers evaluated in the calibration rodeos (Table 6). Each row of data presented in Table 6 represents a unique machine. These machines were all of different age, levels of maintenance, degree of user modification, and standard operating settings thus variation in spray droplet size among the machine was expected. Of the 14 LV-8 sprayers, four were version 1 (LV-8-V1), one was version 2 (LV-8-V2), and nine sprayers contained some modifications of pumps and spray lines that made it difficult to distinguish a specific version. Therefore, all data are presented by individual machine, with no attempt to characterize

Table 2. Effects of a.i. and engine speed on spray atomization for the London Fog model 18–20 sprayer (London Fog, Long Lake, MN).

		Rate per		Droplet size ^y	
Formulation	Engine speed (rpm)	atomizer (gal/min) ²	$ \begin{array}{c} D_{\text{V0.1 y}} \\ (\mu \text{m } \pm \text{sd}) \end{array} $	$D_{V0.5}$ ($\mu m \pm sD$)	$\begin{array}{c} D_{\text{V0.9}} \\ (\mu\text{m} \pm \text{sd}) \end{array}$
Water	2810	0.6	22.3 ± 5.1	57.8 ± 13.2	110.6 ± 22.3
Water + 0.25% NIS ^x	1850	0.6	30.2 ± 2.3	85.9 ± 1.2	214.7 ± 14.8
Diflubenzuron	1500	0.6	38.1 ± 0.4	94.0 ± 2.7	305.5 ± 6.5
Spinetoram	1500	0.6	35.1 ± 0.5	86.4 ± 0.6	260.7 ± 12.9
Fenpropathrin	1350	0.6	38.1 ± 0.7	91.4 ± 0.4	322.2 ± 10.5
Malathion	1350	0.6	37.1 ± 1.0	92.0 ± 0.9	279.2 ± 9.9
Dimethoate	1350	0.6	30.0 ± 2.7	79.6 ± 2.8	205.1 ± 52.7

^z1 gal = 3.7854 L.

Table 3. Effects of a.i. and engine speed on spray atomization for the Curtec sprayer (Curtec of Florida, Vero Beach, FL).

		Rate per		Droplet sizey	
Formulation	Engine speed (rpm)	atomizer (gal/min)²	$D_{V0.1}$ $(\mu m \pm sD)$	$D_{V0.5}$ ($\mu m \pm sd$)	$D_{V0.9}$ ($\mu m \pm sD$)
Water	5100	0.3	41.3 ± 9.4	111.8 ± 12.8	173.6 ± 17.9
Water + 0.25% NIS ^x	5100	0.3	35.3 ± 5.2	94.9 ± 4.6	149.1 ± 4.2
Dimethoate	5100	0.3	37.9 ± 5.9	96.7 ± 11.0	167.3 ± 11.5
Malathion	4800	0.3	31.2 ± 1.3	88.9 ± 0.6	168.7 ± 9.0
Spinetoram	4000	0.3	66.0 ± 23.1	126.4 ± 11.9	200.5 ± 13.1
Diflubenzuron	5100	0.3	39.9 ± 3.7	105.2 ± 6.4	185.5 ± 11.4
Fenpropathrin	4000	0.3	44.3 ± 1.7	113.2 ± 2.9	218.6 ± 33.5

^z1 gal = 3.7854 L.

Table 4. Effects of a.i. and engine speed on spray atomization for the Proptec sprayer (Ledebuhr Industries, Williamston, MI).

		Rate per		Droplet sizey	
Formulation	Engine speed (rpm)	atomizer (gal/min) ^z	$\frac{D_{\text{V0.1}}}{(\mu \text{m} \pm \text{sD})}$	$D_{V0.5}$ ($\mu m \pm sD$)	D _{V0.9} (μm ± sd)
Water	5100	0.36	29.4 ± 0.8	98.4 ± 5.7	161.2 ± 13.6
Water + 0.25% NIS ^x	5100	0.36	33.0 ± 4.2	94.9 ± 15.8	193.0 ± 21.6
Malathion	3500	0.36	33.7 ± 1.6	91.6 ± 4.0	173.6 ± 3.8
Spinetoram	5100	0.36	32.6 ± 2.0	97.6 ± 5.9	165.8 ± 7.0
Diflubenzuron	5100	0.36	31.6 ± 1.1	93.8 ± 3.8	172.9 ± 4.1
Fenpropathrin	3500	0.36	34.5 ± 0.4	96.4 ± 2.1	209.5 ± 11.1

 $^{^{}z}1$ gal = 3.7854 L.

general sprayer model performance. For each machine tested, the droplet size under the initial operational settings is presented followed by the droplet size at the adjusted settings. Typically, for the LV-8 and LV-8-V2, decreasing the engine rpm resulted in increased droplet size such the 90-µm size requirement was met. There were

several of the LV-8 machines that, even with maximum reduction of the engine speed, the 90-µm level was not met. Each of the individual machines tested had unique lower engine speed, again due to variability in machine age, maintenance, and level of modification. For the LV-8-V1 machines tested, similar

adjustments in engine speed did not result in sufficient increase in droplet size. The LV-8-V1 has a smaller pump and small diameter tubing leading to each of the spray nozzles, which limits flow output and thereby the ability to generate larger droplets.

The London Fog model 18–20 citrus sprayers followed similar trends

 $^{^{}y}D_{V.01}^{-}$, $D_{V.05}$, and $D_{V.09}$ = the droplet diameter where 10%, 50%, and 90%, respectively, of the spray volume is contained in droplets smaller than this value. Values represent the mean of three replications; 1 μ m = 1 micron.

^xNIS = nonionic surfactant (R-11; Wilbur-Ellis, Walnut Creek, CA).

 $^{^{}y}D_{v.01}$, $D_{v.05}$, and $D_{v.09}$ = the droplet diameter where 10%, 50%, and 90%, respectively, of the spray volume is contained in droplets smaller than this value. Values represent the mean of three replications; 1 μ m = 1 micron.

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 $^{^{}y}D_{V.01}^{-}$, $D_{V.05}$, and $D_{V.09}$ = the droplet diameter where 10%, 50%, and 90%, respectively, of the spray volume is contained in droplets smaller than this value. Values represent the mean of three replications; 1 μ m = 1 micron.

^{*}NIS = nonionic surfactant (R-11; Wilbur-Ellis, Walnut Creek, CA).

Table 5. Spray droplet size measurements from sprayers in the citrus spray calibration rodeo with the original setting results followed by the adjusted setting results for a water plus nonionic surfactant solution. The sprayers were adjusted to comply with the droplet size requirements of the Special Local Needs permits granted to some insecticides in the State of Florida.

				Original					_
Sprayer ^z	Model no.	Nozzle ^z	Spray rate (gal/acre) ^y	Liquid pressure (psi) ^y	Air pressure (psi)	Engine speed (rpm)	$\frac{D_{\text{V0.1}}}{D_{\text{V0.1}}}$ (\(\mu \text{m} \text{ \text{sD}}\)	plet size in first $D_{V0.5}$ (μ m ± SD)	$\frac{D_{V0.9}}{(\mu m \pm sD)}$
Adapco	190GS	Standard	2		3	2800	17.2 ± 1.5	51.1 ± 5.8	121.4 ± 13.8
AirTec	CAB1000	Albuz	25	70		540 - PTO ^w	37.3 ± 0.3	99 ± 1.2	173.7 ± 4.5
Curtec	648 D	Curtec coarse	10			2100	30.4 ± 0.4	75.5 ± 0.8	133.8 ± 2.3
Curtec	648 D	Curtec fine	10			1500	31.6 ± 1.0	87.1 ± 3.7	159.7 ± 17.6
Curtec	C3000	Curtec coarse	21	15		540 - PTO	27 ± 0.4	70.9 ± 0.6	130.6 ± 4.2
Curtec	P400D	Proptec coarse	2	2		2100	63.2 ± 4.8	149.2 ± 12.2	335.8 ± 79.7
London Fog	2D MaxiPro	Standard	2	1 gal/min ^y	4	2500	17.6 ± 0.2	38.4 ± 0.1	79.4 ± 6.2
ESS	MaxCharge	Standard	15	20	30	440 - PTO	17.0 ± 0.2	30.1 ± 0.1	77.1 ± 0.2
	ESS100			20			14.3 ± 0.3	41.9 ± 0.3	102.9 ± 1.1
Proptec		Proptec	3		7	1700			
		coarse					31.5 ± 1.8	75.5 ± 6.7	147.3 ± 28.1
Proptec		Proptec fine	3		8	1700	31.6 ± 0.4	80.7 ± 4.2	139.3 ± 4.5
Rears	PulBlast	Rotary	5	50		2500	131.6 ± 8.3	278.9 ± 16.9	390.7 ± 25.7
Rears	PulBlast	Albuz ATR-80	5	150		450 - PTO	56.4 ± 0.8	131.4 ± 0.4	214.9 ± 1.0
Sides	Spectrum	Ogee shear	10	42		1700	38.6 ± 2.3	99.7 ± 8.2	184.8 ± 27.4
				Adjusted					
			Targeted	Liquid	Air	Engine		ze after adjust	<u> </u>
0		27 1	rate	pressure	pressure	speed	$D_{V0.1}$	$\mathrm{D_{V0.5}}$	$D_{ m V0.9}$
Sprayer	Model no.	Nozzle	(gal/acre)	(psi)	(psi)	(rpm)	$(\mu m \pm sD)$	(µm ± sd)	$(\mu \mathbf{m} \pm \mathbf{s}\mathbf{D})$
Adapco	190GS	Standard	2	0	3	1900	39.2 ± 1.1	107.6 ± 4.5	227.2 ± 14.8
Curtec	648 D	Curtec coarse	10			1500	31.9 ± 0.8	79.1 ± 1.8	142.1 ± 4.5
Curtec	C3000	Curtec coarse	21	15	0	440 - PTO	33.3 ± 2.1	95.7 ± 2.7	180.2 ± 1.0
London	2D MaxiPro	Standard	2	1 gal/min	4	1640			
Fog							29.4 ± 2.1	76.7 ± 5.6	177 ± 11.5
ESS	MaxCharge	Standard	15	30	25	540 - PTO			
	ESS100						13.3 ± 0.5	34.7 ± 1.4	83.9 ± 3.0
Proptec		Proptec	5	0	7	1300			
		coarse					31.3 ± 1.8	75.5 ± 6.7	147.3 ± 28.1
Proptec		Proptec fine	5	0	7	1300	37.4 ± 2.0	88.7 ± 3.6	162.9 ± 13.1

²Adapco (Sanford, FL); AirTec (AirTec Sprayers, Winter Haven, FL); Curtec (Curtec of Florida, Vero Beach, FL); London Fog (Long Lake, MN); ESS (Electrostatic Spraying Systems, Watkinsville, GA); Proptec (Ledebuhr Industries, Williamston, MI); Rears (Rears Manufacturing, Eugene, OR); Sides (Goldthwaite, TX); Albuz (Spirit River, AB, Canada); Ogee (Spectrum Electrostatic Sprayers, Houston).

as the LV-8s. With a single exception, reducing the engine speed increased $D_{\rm V0.5}$ values such that the 90- μ m size requirement was met.

Conclusions

In response to the need for accurate droplet size assessments of application equipment used in the control of the asian citrus psyllid in Florida, a variety of field application sprayers were evaluated to determine if the applied sprays met the Special Local Needs labeling requirements of volume median diameters of 90 μ m or greater. Initially, a series of studies was conducted across three typical

spray systems and five a.i. to determine typical machine operating characteristics and resulting droplet sizes. From these tests, it was found that for typical air-blast type sprayers, reductions in engine speed were required to reduce air-shear atomization to increase droplet sizes to the required size. For air-assisted sprayers, this also held true with the addition that increased flow rate also potentially increased droplet size. Following these initial assessments, a series of droplet sizing rodeos were held in Florida to measure spray droplet size from applicator- and grower-owned citrus sprayers operating in "as-is"

conditions. Based on the resulting spray droplet size, the sprayer settings were adjusted such that the resulting droplet size would comply with the label requirements. Following the trends seen in the initial round of testing, the majority of the sprayers was adjusted via the engine speed or spray pressure such that the resulting spray's volume median diameter was greater than or equal to 90 µm. As the equipment tested here represent the most typical application equipment used in Florida for asian citrus psyllid control, these results will provide applicators, growers, and extension agents with general guidelines to

yl gal/acre = 9.3540 L·ha⁻¹, 1 psi = 6.8948 kPa, 1 gal = 3.7854 L.

 $^{^{}x}D_{V,01}$, $D_{V,05}$, and $D_{V,09}$ = the droplet diameter where 10%, 50%, and 90%, respectively, of the spray volume is contained in droplets smaller than this value. Values represent the mean of three replications; 1 μ m = 1 micron.

^wPower take-off.

sprayers in the citrus spray calibration rodeo with original setting results followed by the adjusted setting results for a water plus nonionic surfactant solution. The sprayers Table 6. Spray droplet size measurements for Curtis Dyna-Fog LV8 (Curtis Dyna-Fog, Westfield, IN) and London Fog model 18–20 (London Fog, Long Lake, MN) were adjusted to comply with the droplet size requirements of the Special Local Needs permits granted to some insecticides in the State of Florida.

Model Sprayr rate propert Ajr Droplet size* D $V_{0.05}$	loov: •					Origina	Original settings		R	esults after a	Results after adjusting sprayer	•
Model Spray rate pressure Engine speed Dvo.1 Dvo.5 Engine speed Dvo.1 Dvo.5 (pm) (pm + so)	In			Air			Droplet size				Droplet size [*]	
Dyna-Fog LV8 3 6 2560 21.1 ± 2.7 55.5 ± 6.1 130.6 ± 23.9 27.8 ± 0.3 27.8 ± 0.9 Dyna-Fog LV8 3.5 1.0 25.00 21.1 ± 2.7 55.5 ± 6.1 130.6 ± 23.9 27.8 ± 0.9 27.8 ± 0.9 Dyna-Fog LV8 3.5 1.0 25.00 21.1 ± 2.7 55.5 ± 6.1 180.0 27.3 ± 0.3 71.8 ± 0.4 Dyna-Fog LV8 3.5 1.0 25.00 21.4 ± 0.5 35.5 ± 0.1 180.0 27.3 ± 0.3 71.8 ± 0.4 Dyna-Fog LV8 3 7 2600 22.4 ± 0.1 18.5 ± 0.1 180.0 27.3 ± 0.3 71.8 ± 0.4 Dyna-Fog LV8 3 9 2600 22.4 ± 0.1 76.4 ± 0.1 180.0 ± 8.3 190.0 27.3 ± 1.9 98.2 ± 0.1 Dyna-Fog LV8 3 9 2600 24.4 ± 0.7 68.8 ± 2.3 160.9 ± 8.3 11.7 ± 0.1 187.2 ± 1.7 187.2 ± 1.7 187.2 ± 1.7 187.2 ± 1.7 187.2 ± 1.7 187.2 ± 1.7 187.2	9	Model no. ^z	Spray rate (gal/acre)	pressure (psi)y	Engine speed (rpm)	D _{V0.1}	D _{V0.5}	D _{V0.9}	Engine speed (rpm)	D _{V0.1}	D _{V0.5}	D _{V0.9}
Dyna-Pog LV8 5 C 2500 21.1 ± 2.7 C 25.2 ± 6.4 LV9 27.3 ± 0.3 27.3 ± 0.3 27.3 ± 0.3 27.3 ± 0.3 27.3 ± 0.4 27.3 ± 0.3 27.3 ± 0.4 27.3 ± 0.3 27.3 ± 0.4 27.3 ± 0.3 27.3 ±	· i -	1 1/0	2	(L)	7760	326.20	64 E : 11 0	1206 : 220	7760	20.7 - 1.1	67.8.00	210 5 , 10 7
Dyna-Pog LV8 5 6 2500 21.1±2.7 55.5±6.4 112.9±11.4 1800 27.3±0.3 71.8±0.4 Dyna-Pog LV8 3.5 10 2500 16.1±1.6 47.1±3.3 101.7±3.5 1350 35.3±0.3 71.8±0.4 Dyna-Pog LV8 3.5 10 2500 16.1±1.6 47.1±3.3 101.7 35.2±1.0 95.5±6.9 Dyna-Pog LV8 3 7 2600 20.4±0.6 53.1±2.7 106.3±10.3 1800 34.1±0.9 98.9±4.8 Dyna-Pog LV8 3 9 2600 22.4±0.1 64.1±2.1 131.5±16.5 2040 37.3±2.3 113.7±11.9 Dyna-Pog LV8 3 9 2600 22.4±0.1 64.1±2.1 131.5±16.5 2040 37.3±2.3 113.7±11.9 Dyna-Pog LV8 3 2600 26.5±2.1 76.4±4.7 185.4±0.1 1400 42.2±17.7 123.8±13.9 Dyna-Pog LV8 3 2600 26.8±2.3 </td <td>٠,</td> <td>L v 0</td> <td>ו כ</td> <td>) ·</td> <td>0077</td> <td>7.0 H 0.07</td> <td>7.11 H 0.F0</td> <td>7.62 ± 0.001</td> <td>0077</td> <td>Н</td> <td>0. 0 H 0. 7</td> <td>1.7.1 ± 0.7.12</td>	٠,	L v 0	ו כ) ·	0077	7.0 H 0.07	7.11 H 0.F0	7.62 ± 0.001	0077	Н	0. 0 H 0. 7	1.7.1 ± 0.7.12
Dyna-Fog LV8 3.5 10 2500 16.1±1.6 47.1±3.3 101.7±3.5 1350 33.5±1.1 95.5±6.9 Dyna-Fog LV8 2.5 8 2600 16.1±1.6 47.1±3.7 106.3±10.3 1800 28.6±0.6 73.3±2.9 Dyna-Fog LV8 3 7 2600 20.4±0.6 53.1±2.7 106.3±10.3 1800 34.1±0.9 98.9±4.8 Dyna-Fog LV8 3 9 2600 24.8±0.4 76.8±4.4 176.3±19.2 2100 28.6±0.6 73.3±2.3 111.7 Dyna-Fog LV8 3 9 2600 26.8±4.4 176.3±19.2 2120 35.2±0.7 107.2±4.0 Dyna-Fog LV8 3 6 2140 24.4±0.7 69.8±2.3 160.9±8.3 2000 31.1±0.1 98.8±2.7 Dyna-Fog LV8-V1 3 6 2140 24.4±0.7 69.8±2.3 160.9±8.3 2000 31.1±0.1 98.8±2.7 Dyna-Fog LV8-V1 3	Т	Γ N8	ĸ	9	2500	21.1 ± 2.7	+1	112.9 ± 11.4	1800		71.8 ± 0.4	151.4 ± 1.2
LV8 2.5 8 2600 15.8 ± 0.9 39.6 ± 2.1 79.8 ± 7 2100 28.6 ± 0.6 73.3 ± 2.9 LV8 3 7 2600 20.4 ± 0.6 53.1 ± 2.7 106.3 ± 10.3 1800 34.1 ± 0.9 98.9 ± 4.8 LV8 3 7 2600 22.4 ± 0.1 64.1 ± 2.1 131.5 ± 16.5 2040 37.3 ± 2.3 113.7 ± 11.9 LV8 3 9 2600 24.8 ± 0.4 76.3 ± 19.2 2120 37.3 ± 2.3 113.7 ± 11.9 LV8 3 9 2600 24.8 ± 0.4 76.3 ± 19.2 2120 37.2 ± 0.7 107.2 ± 4.0 LV8 1 2 200 24.40 24.4 ± 0.1 24.2 ± 0.1 2120 35.2 ± 0.7 107.2 ± 4.0 LV8-V1 3 6 1670 18.3 ± 0.7 44.2 ± 2.1 90.2 ± 4.3 2300 17.2 ± 0.4 45.7 ± 1.9 LV8-V1 3 6 1670 13.2 ± 1.8 35.3 ± 4.1	П	LV8	3.5	10	2500	16.1 ± 1.6	α	101.7 ± 3.5	1350	33.5 ± 1.1	95.5 ± 6.9	240.1 ± 11.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Dyna-Fog	LV8	2.5	8	2600	15.8 ± 0.9	39.6 ± 2.1	79.8 ± 7	2100		73.3 ± 2.9	154.8 ± 2.8
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Dyna-Fog	LV8	8	_	2600	20.4 ± 0.6	53.1 ± 2.7	106.3 ± 10.3	1800	+1	98.9 ± 4.8	197.3 ± 24.9
LV839 2600 24.8 ± 0.4 76 ± 4.7 185.4 ± 0.1 1400 42.2 ± 1.7 123.8 ± 13.9 LV839 2600 26.5 ± 2.1 76.8 ± 4.4 176.3 ± 19.2 2120 35.2 ± 0.7 107.2 ± 4.0 LV836 2140 24.4 ± 0.7 69.8 ± 2.3 160.9 ± 8.3 2000 31.1 ± 0.1 98.8 ± 2.7 LV8-V12 2600 14.6 ± 0.8 50.1 ± 12.7 157.9 ± 31.3 1600 21.5 ± 0.4 55.6 ± 0.5 LV8-V13 6 1670 18.3 ± 0.7 44.2 ± 2.1 90 ± 1.4 1350 22.1 ± 1.6 56.1 ± 3.8 LV8-V11 7 2600 13.2 ± 1.8 35.3 ± 1.7 69.2 ± 4.3 2300 17.5 ± 0.5 44.8 ± 0.2 LV8-V12 7 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V25 7 2500 27.2 ± 1.6 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V25 7 2500 27.2 ± 1.6 70.9 ± 5.3 2000 24.1 ± 1.1 61.1 ± 2.5 18-200.4 2500 27.2 ± 1.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 18-201 35.0 ± 0.3 18-201.8 2600 31.6 ± 1.6 35.0 ± 0.3 35.0 ± 0.3 35.0 ± 0.3 $35.0 \pm $	Dyna-Fog	LV8	2.4	6	2600	22.4 ± 0.1	64.1 ± 2.1	131.5 ± 16.5	2040	2	113.7 ± 11.9	239.5 ± 33.7
LV8 3 9 2600 26.5 ± 2.1 76.8 ± 4.4 176.3 ± 19.2 2120 35.2 ± 0.7 107.2 ± 4.0 LV8 3 6 2140 24.4 ± 0.7 69.8 ± 2.3 160.9 ± 8.3 2000 31.1 ± 0.1 98.8 ± 2.7 LV8-V1 2 2600 14.6 ± 0.8 50.1 ± 12.7 157.9 ± 31.3 1600 21.5 ± 0.4 55.6 ± 0.5 LV8-V1 3 6 1670 18.3 ± 0.7 44.2 ± 2.1 90 ± 1.4 1350 22.1 ± 1.6 55.1 ± 3.8 LV8-V1 1 7 2600 13.2 ± 1.8 35.3 ± 1.7 69.2 ± 4.3 2300 17.5 ± 0.5 44.8 ± 0.2 LV8-V1 2 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V2 5 7 2500 27.2 ± 1.6 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V2 5 7 2500 12.4 ± 0.6 25.9 ± 2.0	Dyna-Fog	LV8	co	6	2600	24.8 ± 0.4	76 ± 4.7	185.4 ± 0.1	1400		123.8 ± 13.9	277.3 ± 62.7
LV8 3 6 2140 24.4 ± 0.7 69.8 ± 2.3 160.9 ± 8.3 2000 31.1 ± 0.1 98.8 ± 2.7 LV8-V1 2 7 2600 14.6 ± 0.8 50.1 ± 12.7 157.9 ± 31.3 1600 21.5 ± 0.4 55.6 ± 0.5 LV8-V1 3 6 1670 18.3 ± 0.7 44.2 ± 2.1 90 ± 1.4 1350 21.5 ± 0.4 55.6 ± 0.5 LV8-V1 1 7 2600 13.2 ± 1.8 35.3 ± 1.7 69.2 ± 4.3 2000 17.2 ± 0.4 44.8 ± 0.2 LV8-V1 2 7 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V2 5 7 2500 27.2 ± 1.6 76.7 ± 1.4 1900 24.1 ± 1.1 61.1 ± 2.5 LV8-V2 5 7 2500 12.4 ± 0.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 LV8-V2 5 7 2500 $12.4 \pm$	Dyna-Fog	LV8	co	6	2600	26.5 ± 2.1	76.8 ± 4.4	176.3 ± 19.2	2120	35.2 ± 0.7	107.2 ± 4.0	226.8 ± 11.0
LV8-V1 2 7 2600 14.6 ± 0.8 50.1 ± 12.7 157.9 ± 31.3 1600 21.5 ± 0.4 55.6 ± 0.5 LV8-V1 3 6 1670 18.3 ± 0.7 44.2 ± 2.1 90 ± 1.4 1350 22.1 ± 1.6 56.1 ± 3.8 LV8-V1 1 7 2600 13.2 ± 1.8 35.3 ± 1.7 69.2 ± 4.3 2300 17.5 ± 0.5 44.8 ± 0.2 LV8-V1 2 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V1 2 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V2 5 7 2600 12.4 ± 0.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 LV8-V2 1 2500 12.4 ± 0.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 18-20 1 25.0 25.8 ± 0.7 25.0 25	Dyna-Fog	LV8	8	9	2140	24.4 ± 0.7	69.8 ± 2.3	160.9 ± 8.3	2000	31.1 ± 0.1	98.8 ± 2.7	242.3 ± 38.9
LV8-V1 3 6 1670 18.3 ± 0.7 44.2 ± 2.1 90 ± 1.4 1350 22.1 ± 1.6 56.1 ± 3.8 LV8-V1 1 7 2600 13.2 ± 1.8 35.3 ± 1.7 69.2 ± 4.3 2300 17.5 ± 0.5 44.8 ± 0.2 LV8-V1 2 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V1 2 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V2 5 7 2500 27.2 ± 1.6 76.7 ± 1.5 166.7 ± 21.4 2020 33.1 ± 2.6 97.3 ± 1.8 18-20 0.4 2600 12.4 ± 0.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 18-20 1 46.8 ± 0.1 85.0 ± 0.3 1800 48.1 ± 0.8 117.9 ± 0.1 18-20 1.8 2 22.8 ± 0.7 62.0 ± 0.1 130.6 ± 3.5 1800 48.1 ± 0.8 177.9 ± 0.1 18-20 1.8 2<	Dyna-Fog	LV8-V1	2	^	2600	14.6 ± 0.8	50.1 ± 12.7	157.9 ± 31.3	1600	21.5 ± 0.4	55.6 ± 0.5	117.4 ± 2.4
LV8-V1 1 7 2600 13.2 ± 1.8 35.3 ± 1.7 69.2 ± 4.3 2300 17.5 ± 0.5 44.8 ± 0.2 LV8-V1 2 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V2 5 7 2500 27.2 ± 1.6 76.7 ± 1.5 166.7 ± 21.4 2020 33.1 ± 2.6 97.3 ± 1.8 LV8-V2 5 7 2500 12.4 ± 0.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 118.2 18-20 1 2850 12.4 ± 0.6 25.9 ± 0.1 85.0 ± 0.3 1800 24.1 ± 1.1 61.1 ± 2.5 118.2 18-20 1 27.2 27.2 27.2 27.8 ± 0.7 <	Dyna-Fog	LV8-V1	co	9	1670	18.3 ± 0.7	44.2 ± 2.1	90 ± 1.4	1350	+1	56.1 ± 3.8	112.2 ± 12.8
LV8-V1 2 7 2600 14.2 ± 0.8 35.4 ± 1.9 70.9 ± 5.3 2000 17.2 ± 0.4 45.7 ± 1.9 LV8-V2 5 7 2500 27.2 ± 1.6 76.7 ± 1.5 166.7 ± 21.4 2020 33.1 ± 2.6 97.3 ± 1.8 LV8-V2 5 7 2500 27.2 ± 1.6 76.7 ± 1.5 166.7 ± 21.4 2020 33.1 ± 2.6 97.3 ± 1.8 18-20 0.4 2600 12.4 ± 0.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 18-20 1 2850 18.9 ± 0.1 46.8 ± 0.1 85.0 ± 0.3 1800 48.1 ± 0.8 117.9 ± 0.1 18-20 2 2 22.8 \pm 0.7 62.0 ± 0.1 130.6 ± 3.5 1800 48.1 ± 0.8 117.9 ± 0.1 18-20 1.8 2600 31.6 ± 1.6 83.1 ± 3.7 177.9 ± 13.9 2400 35.2 ± 3.4 18-20 3 4 2500 24.9 ± 5.6 65.1 ± 17.7 134.7 ± 23.8 1	Dyna-Fog	LV8-V1	1	^	2600	13.2 ± 1.8	35.3 ± 1.7	69.2 ± 4.3	2300	17.5 ± 0.5	44.8 ± 0.2	88.1 ± 2.5
LV8-V2 5 7 2500 27.2 ± 1.6 76.7 ± 1.5 166.7 ± 21.4 2020 33.1 ± 2.6 97.3 ± 1.8 18-20 0.4 2600 12.4 ± 0.6 25.9 ± 2.0 57.1 ± 18.4 1900 24.1 ± 1.1 61.1 ± 2.5 18-20 1 2850 18.9 ± 0.1 46.8 ± 0.1 85.0 ± 0.3 1800 24.1 ± 1.1 61.1 ± 2.5 18-20 1 2850 18.9 ± 0.1 46.8 ± 0.1 85.0 ± 0.3 1800 48.1 ± 0.8 117.9 ± 0.1 18-20 2 2720 22.8 ± 0.7 62.0 ± 0.1 130.6 ± 3.5 1800 48.1 ± 0.8 117.9 ± 0.1 18-20 1.8 2600 31.6 ± 1.6 83.1 ± 3.7 177.9 ± 13.9 2400 35.2 ± 0.6 93.2 ± 3.4 18-20 3 4 2500 24.9 ± 5.6 65.1 ± 17.7 134.7 ± 23.8 1500 49.1 ± 1.9 124.4 ± 6.1	Dyna-Fog	LV8-V1	2	_	2600	14.2 ± 0.8		70.9 ± 5.3	2000	+1	+1	93.5 ± 7.6
	Dyna-Fog	LV8-V2	ъ	^	2500	27.2 ± 1.6	+1	166.7 ± 21.4	2020		97.3 ± 1.8	234.2 ± 16.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	London Fog	18–20	0.4		2600	12.4 ± 0.6	25.9 ± 2.0		1900	24.1 ± 1.1	61.1 ± 2.5	104.2 ± 4.5
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	London Fog	18–20	1		2850	18.9 ± 0.1	46.8 ± 0.1	85.0 ± 0.3	1800	37.0 ± 0.4	90.3 ± 1.9	167.0 ± 9.6
$18-20 \qquad 1.8 \qquad 2600 \qquad 31.6 \pm 1.6 \qquad 83.1 \pm 3.7 \qquad 177.9 \pm 13.9 \qquad 2400 \qquad 35.8 \pm 2.3 \qquad 96.1 \pm 3.1 \\ 18-20 \qquad 1.8 \qquad 2600 \qquad 32.2 \pm 2.6 \qquad 89.9 \pm 4.0 \qquad 190.2 \pm 4.4 \qquad 2400 \qquad 30.2 \pm 0.6 \qquad 93.2 \pm 3.4 \\ 18-20 \qquad 3 \qquad 4 \qquad 2500 \qquad 24.9 \pm 5.6 \qquad 65.1 \pm 17.7 \qquad 134.7 \pm 23.8 \qquad 1500 \qquad 49.1 \pm 1.9 \qquad 124.4 \pm 6.1 $	London Fog	18–20	7	^	2720	22.8 ± 0.7	62.0 ± 0.1	130.6 ± 3.5	1800		117.9 ± 0.1	237.8 ± 4.0
$18-20 \qquad 1.8 \qquad 2600 \qquad 32.2 \pm 2.6 89.9 \pm 4.0 190.2 \pm 4.4 \qquad 2400 \qquad 30.2 \pm 0.6 93.2 \pm 3.4 \\ 18-20 \qquad 3 \qquad 4 \qquad 2500 \qquad 24.9 \pm 5.6 65.1 \pm 17.7 134.7 \pm 23.8 \qquad 1500 \qquad 49.1 \pm 1.9 124.4 \pm 6.1$	London Fog	18–20	1.8		2600	31.6 ± 1.6	83.1 ± 3.7	177.9 ± 13.9	2400	± 2	96.1 ± 3.1	202.4 ± 15.8
$18-20$ 3 4 2500 24.9 ± 5.6 65.1 ±17.7 134.7 ± 23.8 1500 49.1 ± 1.9 124.4 ± 6.1	London Fog	18–20	1.8		2600	32.2 ± 2.6	+1	190.2 ± 4.4	2400	30.2 ± 0.6	93.2 ± 3.4	221.6 ± 26.7
	London Fog	18–20	co	4	2500	24.9 ± 5.6	+1	+1	1500	+1	+1	246.5 ± 7.6

D_{V,01}, D_{V,09} and D_{V,09} the droplet diameter where 10%, 50%, and 90%, respectively, of the spray volume is contained in droplets smaller than this value. Values represent the mean of three replications; 1 µm = 1 micron 2 LV8 and LV8-V2 have 3 /8- to 1/2-inch tubing to each nozzle, LV8-V1 has 1/8-inch tubing to each nozzle; 1 inch = 2.54 cm. 3 gal/acre = 9.3540 Lha⁻¹; 1 psi = 6.8948 kPa.

insure that spray systems are operated in a manner that complies with label restrictions.

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Appendix





USDA - ARS - Aerial Application Technology Group College Station, TX Nozzles, Aug 2009

HELOS (H1780) & SPRAYER, R5: 0.5/4.5...875μm

2009-09-02, 07:2 .:.,...

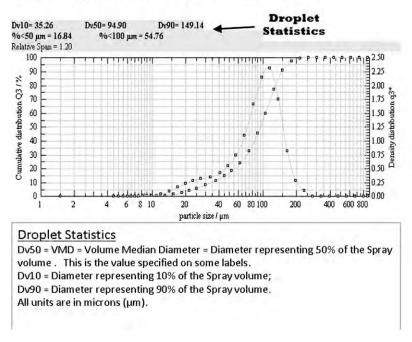


Fig. 2. Handout given to applicators at the citrus sprayer calibration rodeos to explain the results of the tests; $1 \mu m = 1 \text{ micron}$, 1 gal = 3.7854 L, 1 psi = 6.8948 kPa, $1 \text{ m/s} = 1 \text{ m·s}^{-1} = 2.2369 \text{ mph}$.